

## Helicity effect on turbulent passive and active scalar diffusivities

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### ABSTRACT

10  
11 Turbulent flows are known to produce enhanced effective magnetic and passive scalar diffusivities,  
12 which can fairly accurately be determined with numerical methods. It is now known that, if the flow  
13 is also helical, the effective magnetic diffusivity is reduced relative to the nonhelical value. Neither the  
14 usual second-order correlation approximation nor the various  $\tau$  approaches have been able to capture  
15 this. Here we show that the helicity effect on the turbulent passive scalar diffusivity works in the  
16 opposite sense and leads to an enhancement. We have also demonstrated that the correlation time  
17 of the turbulent velocity field increases by the kinetic helicity. This is a key point in the theoretical  
18 interpretation of the obtained numerical results. Simulations in which helicity is being produced self-  
19 consistently by stratified rotating turbulence resulted in a turbulent passive scalar diffusivity that was  
20 found to be decreasing with increasing rotation rate.

21 *Keywords:* Astrophysical magnetism (102) — Magnetic fields (994)

### 22 1. INTRODUCTION

23 In many astrophysical plasmas such as stellar convec-  
24 tion zones, the interstellar medium, and accretion discs,  
25 the Reynolds numbers are extremely large. Therefore,  
26 to describe the large-scale behavior of such flows, one of-  
27 ten replaces the small viscosity or diffusion coefficients  
28 by effective ones. Turbulent diffusivities in the evolution  
29 equations for passive scalars act similarly as ordinary  
30 (molecular or atomic) ones, except that they character-  
31 ize the diffusion of larger scale structures, as described  
32 by the corresponding averaged or coarse-grained evolu-  
33 tion equations. Denoting the mean passive scalar con-  
34 centration  $C$  by an overbar, the equation for  $\overline{C}$  is given  
35 by

$$36 \frac{\partial \overline{C}}{\partial t} = -\nabla \cdot (\overline{U} \overline{C}) + (\kappa + \kappa_t) \nabla^2 \overline{C}, \quad (1)$$

37 where we have allowed for the possibility of a mean flow  
38  $\overline{U}$ , while  $\kappa$  and  $\kappa_t$  are the microphysical and turbulent  
39 diffusion coefficients, respectively. The diffusion coeffi-

40 cients are proportional to the product of the mean free  
41 path and the typical velocity of particles or, in the tur-  
42 bulent case, the product of the integral turbulent scale  
43 and the rms velocity. Equation (1) is written for turbu-  
44 lence without stratification of the mean density or tem-  
45 perature, so that effective pumping velocity caused by  
46 the turbulent thermal diffusion vanishes (Elperin et al.  
47 1997; Rogachevskii 2021).

48 The derivation of the turbulent diffusion coefficients  
49 is usually done by some approximations. Meanwhile,  
50 significant progress has been made by numerically com-  
51 puting these turbulent coefficients. A particularly useful  
52 approach is the test-field method (Schrunner et al. 2005,  
53 2007), which was originally applied to magnetic fields  
54 in spherical geometry and then to Cartesian domains  
55 (Brandenburg 2005; Brandenburg et al. 2008). This  
56 method is sufficiently accurate to identify subtle effects  
57 caused by kinetic helicity in the flow (Brandenburg et al.  
58 2017).

59 In the presence of magnetic fields, the kinetic heli-  
60 city causes completely new qualities of its own. Unlike  
61 the case of turbulent or microphysical diffusion, helicity

also produces non-diffusive effects that lead to a destabilization of the non-magnetic state. This is because helicity is a pseudo-scalar, which can couple the axial magnetic field vector with the polar electric field vector to give an extra contribution to the turbulent electromotive force in the mean-field induction equation. By contrast, the turbulent magnetic diffusivity is an ordinary scalar. It was therefore surprising when kinetic helicity was found to affect even the magnetic diffusivity (Brandenburg et al. 2017). This effect was such that helicity suppresses the magnetic diffusivity by a certain amount. The possibility of a helicity effect on the turbulent magnetic diffusivity was already noticed in the early work of Nicklaus & Stix (1988), but they found an enhancement of the turbulent magnetic diffusivity by the kinetic helicity.

Applying the Feynman diagram technique, Dolginov & Silant'ev (1987) show that kinetic helicity can increase the turbulent diffusion of a passive scalar field. On the other hand, subsequent work by Zhou (1990) using renormalization-group theory found no effect of helicity on the renormalized eddy viscosity. The effect of kinetic helicity on passive scalar diffusion was also investigated by Chkhetiani et al. (2006) using the renormalization group approach. They found that the effective diffusivity can be 50% larger in the helical case. They also noted that there is no helicity effect on the anomalous scaling of the structure functions.

The results of Brandenburg et al. (2017) were recently verified by Mizerski (2023) using the renormalization group approach. In particular, he found that for small magnetic Reynolds numbers, the helical correction to turbulent diffusion of the mean magnetic field is proportional to  $\text{Re}_M^2 (H_K \tau_c)^2 / \langle \mathbf{u}^2 \rangle$ , where  $\text{Re}_M = \tau_c \langle \mathbf{u}^2 \rangle / \eta$  is the magnetic Reynolds number,  $\tau_c$  is the turbulent correlation time,  $\eta$  is the magnetic diffusion caused by an electrical conductivity of plasma, and  $H_K = \langle \mathbf{u} \cdot \boldsymbol{\omega} \rangle$  is the kinetic helicity. This scaling ( $\propto \text{Re}_M^2$ ) is shown in Figure 4 of Brandenburg et al. (2017). This confirms that the helical correction cannot emerge from the second-order correlation approximation, where the transport coefficients are only linear in the magnetic Reynolds number.

What has not yet been specifically addressed is the effect of helicity on the passive scalar diffusivity, or even the thermal diffusivity of an active scalar such as the temperature or the specific entropy in the mean-field energy equation. Doing this is the purpose of the present work.

Helicity affects the value of the turbulent passive and active scalar diffusivity in a clear and consistent way. This is similar to the helicity effect on the turbulent

magnetic diffusivity, but this new effect is the other way around, i.e., the turbulent passive and active scalar diffusion is enhanced by helicity, while the turbulent magnetic diffusivity is decreased. In the accompanying theoretical paper by Rogachevskii et al. (2025), remaining puzzles are addressed and possible explanations are being proposed.

Of some interest in this context is the earlier work of Brandenburg et al. (2012), who computed turbulent magnetic field and passive scalar transport for rotating stratified turbulence. The combined presence of rotation and stratification also leads to helicity and therefore to an  $\alpha$  effect. They found a slight decrease of the magnetic diffusivity as the angular velocity is increased. At the time, this was not thought surprising because the focus was on new turbulent transport coefficients that only arise because of rotation and stratification. Furthermore, already rotation alone (without helicity) is known to decrease the turbulent magnetic diffusivity (Rädler et al. 2003).

For most astrophysical purposes, only order of magnitude estimates of turbulent transport coefficients are usually considered. This may change in future, when more accurate methods and measurements become more commonly available both in simulations and in observations. For example, the discrepancy in the estimate for the turbulent magnetic diffusivity was noticed in theoretical work in high-energy astrophysics on the chiral magnetic effect when simple estimates for the turbulent magnetic diffusivity did not match previous estimates (Schober et al. 2018). This discrepancy was then explained by the presence of helicity in one of the cases.

## 2. OUR MODEL

We consider both isothermal and non-isothermal turbulence and begin with the former.

### 2.1. Basic equations for isothermal turbulence

Our basic equations are the induction and passive scalar equations for the magnetic field  $\mathbf{B}$  and the passive scalar concentration  $C$  (e.g., number density of particles). The magnetic field is also divergence-free. The governing equations are then

$$\frac{\partial \mathbf{B}}{\partial t} = \nabla \times (\mathbf{U} \times \mathbf{B} - \mathbf{E}_{\text{diff}}), \quad \mathbf{E}_{\text{diff}} = -\eta \nabla \times \mathbf{B}, \quad (2)$$

$$\frac{\partial C}{\partial t} = \nabla \cdot (-\mathbf{U}C - \mathbf{F}_{\text{diff}}), \quad \mathbf{F}_{\text{diff}} = -\kappa \nabla C. \quad (3)$$

The velocity  $\mathbf{U}$  is obtained as a solution of the Navier-Stokes equations. In the kinematic test-field method, we ignore the feedback of the magnetic field on the flow, i.e., we solve

$$\frac{D\mathbf{U}}{Dt} = -c_s^2 \nabla \ln \rho + \mathbf{f} + \frac{1}{\rho} \nabla \cdot (2\rho\nu\mathbf{S}), \quad (4)$$

$$\frac{D \ln \rho}{Dt} = -\nabla \cdot \mathbf{U}. \quad (5)$$

where  $\rho$  is the density,  $c_s$  is the isothermal sound speed,  $\nu$  is the kinematic viscosity,  $\mathbf{S}$  is the rate of strain tensor with the components  $S_{ij} = (\partial_i u_j + \partial_j u_i)/2 - \delta_{ij} \nabla \cdot \mathbf{u}/3$ , and  $\mathbf{f}$  represents a forcing function that is  $\delta$ -correlated in time and consists of plane waves with a mean forcing wavenumber  $k_f$ . It is given by  $f_i = R_{ij} f_j^{(\text{nohel})}$ , where  $R(\hat{\mathbf{k}}) = (\delta_{ij} - \sigma \epsilon_{ijk} \hat{k}_k)/\sqrt{1 + \sigma^2}$  depends on  $\hat{\mathbf{k}} = \mathbf{k}/k$  with  $k = |\mathbf{k}|$  and the fractional helicity  $\sigma$ , and  $\mathbf{f}^{(\text{nohel})} = f_0 \mathbf{e} \times \mathbf{k}/|\mathbf{e} \times \mathbf{k}|$  is a nonhelical forcing function with  $f_0$  being a scaling factor and  $\mathbf{e}$  a random vector that is not aligned with  $\mathbf{k}$ .

## 2.2. Equations for non-isothermal turbulence

In our simulations of non-isothermal turbulence, we measure the response of the system to imposing large-scale gradient of specific entropy  $s$  with a relaxation time  $\tau$ . The evolution equations for  $\mathbf{u}$  and  $s$  are then

$$\frac{D\mathbf{U}}{Dt} = -c_s^2 \nabla (\ln \rho + s/c_p) + \mathbf{f} + \frac{1}{\rho} \nabla \cdot (2\rho\nu\mathbf{S}), \quad (6)$$

$$T \frac{Ds}{Dt} = 2\nu\mathbf{S}^2 + \frac{1}{\rho} (\nabla \cdot \mathbf{F}_{\text{rad}} - \mathcal{C}) - \frac{s - \tilde{s}_0}{\tau}, \quad (7)$$

where  $T$  is the temperature,  $c_p$  is the specific heat at constant pressure,  $\mathbf{F}_{\text{rad}} = -c_p \rho \chi \nabla T$  is the radiative flux, and  $\mathcal{C}$  is a volumetric cooling function to compensate for viscous heating. Since the system is no longer isothermal, the sound speed is now given by  $c_s^2 = (\gamma - 1)c_p T$ , where  $\gamma = c_p/c_v$  is the ratio of specific heats, and  $c_v$  is the specific heat at constant volume. For the target profile of specific entropy, we choose  $\tilde{s}_0 = s_0 \sin k_T z$ . Here, we take  $k_T = k_1$  for what will later be called the test-field wavenumber, where  $k_1 = 2\pi/L$  is the smallest wavenumber in the domain. Different values of  $k_T$  would be of interest for studying the scale dependence of turbulent transport, as has been done on various occasions (Brandenburg & Sokoloff 2002; Brandenburg et al. 2008, 2009).

## 2.3. Parameters

For the scale separation ratio, i.e., the ratio of the forcing wavenumber  $k_f$  and the box wavenumber  $k_1$ , we take  $k_f/k_1 = 5.1$  in most of our cases. Although not stated explicitly there, this was also the value adopted in Brandenburg et al. (2017). Larger (smaller) values of  $k_f$  allow us to access larger (smaller) scale separation ratios. At the end of this paper, we present a small survey of different choices; see also Brandenburg et al. (2008, 2009) for such studies in other contexts. Our main governing control parameters are the Reynolds number  $\text{Re} = u_{\text{rms}}/\nu k_f$  and the Mach number  $\text{Ma} = u_{\text{rms}}/c_s$ .

The Schmidt number,  $\text{Sc} = \nu/\kappa$ , the magnetic Prandtl number,  $\text{Pr}_M = \nu/\eta$ , and the thermal Prandtl number  $\text{Pr} = \nu/\chi$  are unity in all cases. Therefore, the magnetic Reynolds number  $\text{Re}_M = u_{\text{rms}}/\eta k_f$  and the Péclet number  $\text{Pe} = u_{\text{rms}}/\chi k_f$  equal the fluid Reynolds number in all cases.

## 2.4. Test-field methods

The test-field method implies the simultaneous solution of additional equations for the fluctuating magnetic field or the fluctuating passive scalar concentration. The variables are indicated by the letter  $T$ . The equations are obtained by subtracting the corresponding averaged equations from the original ones and yield

$$\frac{\partial \mathbf{b}^T}{\partial t} = \nabla \times (\mathbf{u} \times \overline{\mathbf{B}^T} + \overline{\mathbf{U}} \times \mathbf{b}^T + \mathcal{E}'_T) + \eta \nabla^2 \mathbf{b}^T, \quad (8)$$

$$\frac{\partial c^T}{\partial t} = \nabla \cdot (-\mathbf{u} \overline{\mathbf{C}^T} - \overline{\mathbf{U}} c^T + \mathcal{F}'_T) + \kappa \nabla^2 c^T, \quad (9)$$

where  $\mathcal{E}'_T = \mathbf{u} \times \mathbf{b} - \overline{\mathbf{u} \times \mathbf{b}}$  and  $\mathcal{F}'_T = -(\mathbf{u}c - \overline{\mathbf{u}c})$  are non-linear terms that are neglected in the second-order correlation approximation. Including those terms yields the new subtle effects that we found in Brandenburg et al. (2017) for  $\eta_t$  and in the present work for  $\kappa_t$ .

In the following, we assume planar averages and denote them by overbars, e.g.,  $\overline{\mathbf{B}}(z, t) = \int \mathbf{B}(x, y, z, t) dz/L_\perp^2$ , where  $L_\perp$  is the extent of the computational domain in the  $xy$  plane. In the spirit of the test-field method, one decouples Equations (8) and (9) from those for the actual fluctuations and solve them for a set of mean fields (mean scalars) such that one can compute  $\alpha_{ij}$ ,  $\eta_{ij}$ , and  $\kappa_{ij}$  uniquely for each time step and at each value of  $z$ . Using as a shorthand  $s = \sin k_T z$  and  $c = \cos k_T z$ , we choose sinusoidal and cosinusoidal test fields  $\overline{\mathbf{B}}^1 = (s, 0, 0)$ ,  $\overline{\mathbf{B}}^2 = (c, 0, 0)$ ,  $\overline{\mathbf{B}}^3 = (0, s, 0)$ , and  $\overline{\mathbf{B}}^4 = (0, c, 0)$ , as well as  $\overline{\mathbf{C}}^1 = s$ ,  $\overline{\mathbf{C}}^2 = c$ , i.e., four different test fields for  $\overline{\mathbf{B}}^T$  and two different ones for  $\overline{\mathbf{C}}^T$ . This allows us to compute the coefficient  $\alpha_{ij}$ ,  $\eta_{ij}$ , and  $\kappa_{ij}$  in the parameterizations

$$\overline{\mathcal{E}}_i^T = \alpha_{ij} \overline{\mathbf{B}}_j^T - \eta_{ij} (\nabla \times \overline{\mathbf{B}}^T)_j, \quad (10)$$

$$\overline{\mathcal{F}}_i^T = \gamma_i \overline{\mathbf{C}}^T - \kappa_{ij} \nabla_j \overline{\mathbf{C}}^T, \quad (11)$$

where  $\overline{\mathcal{E}}^T = \overline{\mathbf{u} \times \mathbf{b}_T}$ ,  $\overline{\mathcal{F}}^T = -\overline{\mathbf{u}c_T}$ , and  $i, j = 1, 2$  denote the  $x$  and  $y$  components. The aforementioned turbulent viscosity and passive scalar diffusivity are then given by  $\eta_t = (\eta_{11} + \eta_{22})/2$  and  $\kappa_t = (\kappa_{11} + \kappa_{22})/2$ . The effective pumping velocity  $\gamma$  of the mean magnetic field vanishes for homogeneous turbulence, but the effective pumping velocity  $\gamma$  of the mean passive scalar field due to the density stratification of the fluid (Elperin et al.

1997; Rogachevskii 2021) was found to lead to downward transport of the mean passive scalar concentration (to the maximum of the mean fluid density) in density stratified turbulence (Brandenburg et al. 2012; Haugen et al. 2012).

It should be noted that in the original application of the test-field method, Schrunner et al. (2005, 2007) used a combination of constant and linearly varying test fields. This choice is appropriate for computing turbulent transport properties on the largest possible scales, but it is not well suited for the use in periodic domains. This was the main reason why Brandenburg (2005) employed sinusoidal and cosinusoidal test fields, but it also provided a natural way of computing the dependence of the turbulent transport coefficients on different length scales or for different wavenumbers. The resulting formulation of the electromotive force in Fourier space translates directly into one in terms of integral kernels (Brandenburg et al. 2008). This allowed us to avoid the restriction to large scale separation in space and time by replacing the multiplications with turbulent transport coefficients by a convolution with the appropriate integral kernels; see Hubbard & Brandenburg (2009) and Rheinhardt & Brandenburg (2012) for corresponding studies. The effect of different spatial scales on turbulent mixing was also investigated by de Avillez & Mac Low (2002) using checkerboard patterns, but this approach cannot so easily be utilized in the framework of mean-field theory.

### 2.5. Active scalar diffusivity

To determine the turbulent radiative diffusion coefficient, we use the standard mean-field expression for the enthalpy flux (Rüdiger 1989),

$$\overline{\mathcal{F}}_{\text{enth}} = -\chi_t \overline{\rho T \nabla S}, \quad (12)$$

where the actual enthalpy flux is computed as  $\overline{\mathcal{F}}_{\text{enth}} = \overline{(\rho \mathbf{U})' c_p T'}$ , and correlate their  $z$  components against each other to determine  $\chi_t$ . Here, primes denote the departures from the horizontal means. This method follows that employed by Käpylä & Singh (2022), who also computed the turbulent kinematic viscosity in an analogous way by correlating the  $yz$  component of the Reynolds stress against the corresponding component of the mean-field strain tensor. The current setup differs from that in Käpylä & Singh (2022) in that a large-scale velocity is not imposed and therefore no off-diagonal Reynolds stress is present. The emergence of such off-diagonal components in shear flows was studied by Mitra et al. (2009), who found an increase of the turbulent magnetic diffusivity.

### 2.6. Simulations, data, and error bars

We use the PENCIL CODE for our simulations (Pencil Code Collaboration et al. 2021). It uses sixth order accurate spatial derivatives and a third order timestepping scheme. It also allows us to compute turbulent transport coefficients with the test-field method. For that purpose, we invoke the modules `testfield_z` and `testscalar` within the PENCIL CODE.

We present our results for  $\alpha$ ,  $\eta_t$ , and  $\kappa_t$  in normalized form and divide  $\alpha$  by  $A_0 = u_{\text{rms}}/3$  and  $\eta_t$  and  $\kappa_t$  by  $D_0 = u_{\text{rms}}/3k_f$ . This allows us to compare runs with different rms velocity amplitudes.

Our results for the turbulent transport coefficients are functions of  $z$  and  $t$ . Since the turbulence in our simulations is homogeneous, we average the resulting transport coefficients over  $z$ . The resulting time series is then averaged over statistically steady intervals and error bars have been estimated by taking the largest departure to the average from any one third of the full time series. For sufficiently long time series, the resulting errors are rather small, so we often exaggerate them by a factor of 3 or 4, as is indicated in the plots below.

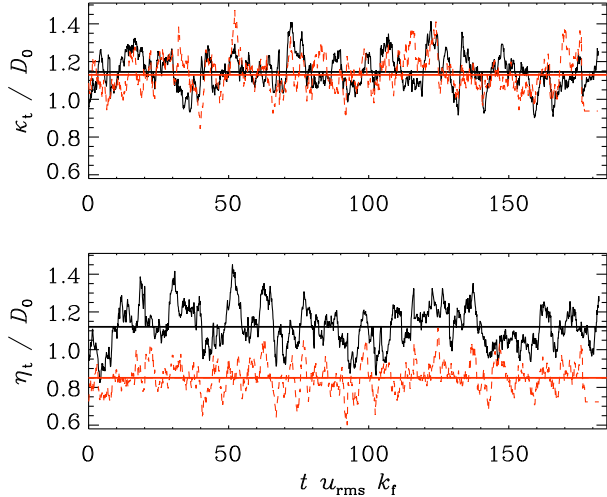
## 3. RESULTS

### 3.1. Passive scalar results and comparison

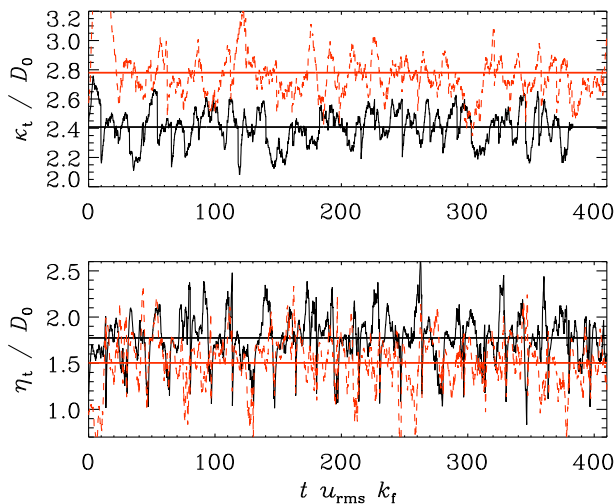
Although the results for  $\eta_t$  have already been computed in Brandenburg et al. (2017), we compute them here again by invoking similar test-field routines in the PENCIL CODE at the same time. The test-field method for passive scalars was already described in Brandenburg et al. (2009). Rädler et al. (2011) applied it to passive scalar diffusion in compressible flows. In the following, we use  $u_{\text{rms}}$  and  $k_f$  to express our results in nondimensional form by normalizing the diffusivities by  $u_{\text{rms}}/3k_f$ . Using earlier test-field results, this was found to be an accurate estimate (Sur et al. 2008).

Figure 1 shows a comparison of time series of  $\kappa_t$  and  $\eta_t$  for nonhelical and helical cases and  $\text{Re} = 2.4$ . While  $\kappa_t$  appears to be unaffected by the presence of helicity,  $\eta_t$  is suppressed, as already found by Brandenburg et al. (2017). For  $\text{Re} = 120$ , however,  $\kappa_t$  is found to be *enhanced* by the presence of helicity; see Figure 2. We have considered a number of additional simulations with other values of  $\text{Re}$ . The dependence on  $\text{Re}$  is shown in Figure 3; see also Table 1 for a summary. The trend in  $\eta_t$  does not follow a smooth dependence, suggesting that statistical noise or other unaccounted factors may have influenced the results.

The forcing is kept constant between different runs, so the resulting rms velocity depends on how stiff the system is against this forcing. We see that the value of the Mach number increases slightly with increasing values of the Reynolds number. We also see that the Mach num-



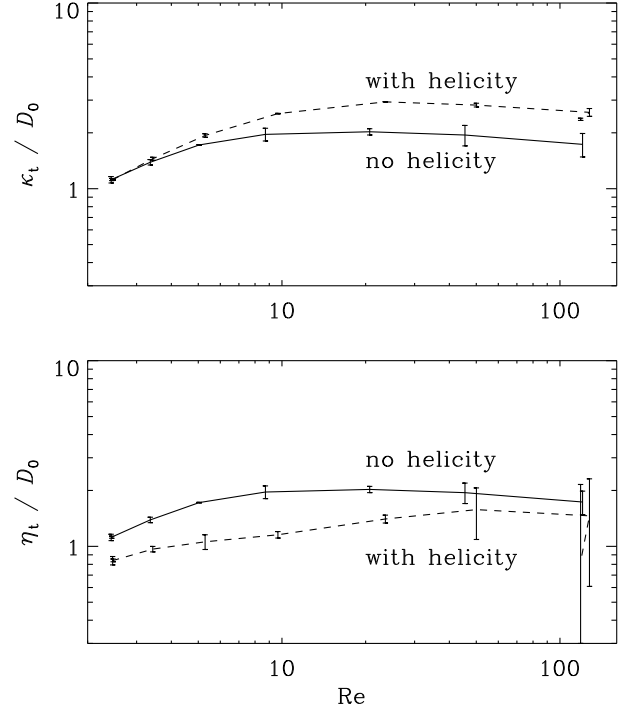
**Figure 1.** Time series of  $\kappa_t$  (upper panel) and  $\eta_t$  (lower panel) for Runs A without helicity (solid black line) and with helicity (dashed red line) with  $Re = 2.4$ . The thick black and red horizontal lines denote the time-averaged values.



**Figure 2.** Similar to Figure 1, but for Runs F with  $Re = 120$ .

358 ber is slightly enhanced in the simulations with helical  
 359 forcing. This suggests that such flows are less effective  
 360 in dissipating energy. These slight changes in  $Ma$  do not  
 361 significantly affect our results for  $\eta_t$  and  $\kappa_t$ , because we  
 362 always present our results in normalized form and we  
 363 are here only interested in subsonic turbulence. Note  
 364 also that the compressibility of the turbulence affects  
 365 only non-helical contributions to the turbulent diffusion  
 366 (Rogachevskii et al. 2018).

367 In Appendix A, we compare our results with different  
 368 degrees of helicity with earlier simulations of rotating  
 369 stratified turbulence in which helicity is automatically



**Figure 3.** Reynolds number dependence of  $\kappa_t$  (upper panel) and  $\eta_t$  (lower panel) for nonhelical (solid lines) and helical (dashed lines). The error bars have been exaggerated by a factor of 3.

370 being produced in self-consistent way. It turns out, how-  
 371 ever, that the enhancement of turbulent diffusion by helicity  
 372 is not being reproduced in such simulations. We  
 373 argue that this is caused by the more dominant effect of  
 374 rotation which strongly suppresses turbulent transport.

### 3.2. Active scalar results

375  
 376 The results of simulations similar to those of  
 377 Käpylä & Singh (2022) are shown in Figure 4. Here we  
 378 see the turbulent heat diffusivity computed from an im-  
 379 posed entropy gradient (see Käpylä & Singh 2022, for  
 380 details) for non-helical and helical cases. For  $Pe = Re >$   
 381 10, there is a statistically significant increase of  $\chi_t$  by  
 382 about 10% for the helical cases relative to the nonheli-  
 383 cal ones. These results were obtained by correlating the  
 384 actual enthalpy flux with the mean-field expression given  
 385 by Equation (12). In Käpylä & Singh (2022), an alter-  
 386 native independent method was used where the mean  
 387 entropy profile is initially forced and then allowed to  
 388 decay. This yielded very similar results.

389 The kinetic helicity effects on turbulent diffusion of the  
 390 mean magnetic and scalar fields are partially related to  
 391 the helicity effect on the effective correlation time. To  
 392 examine this in more detail, we compute the correlation

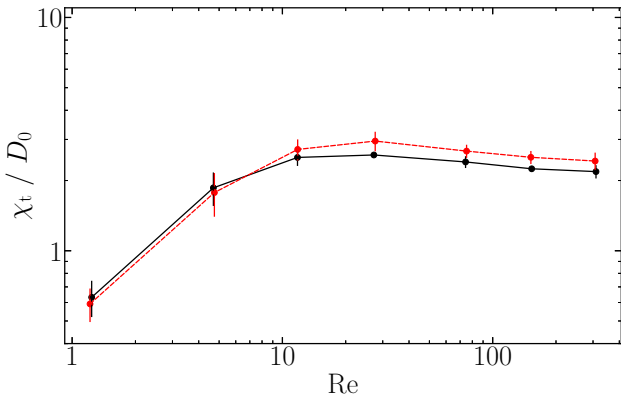


**Table 1.** Values of  $\kappa_t^{\text{nhel}}$  and  $\kappa_t^{\text{hel}}$  as well as  $\eta_t^{\text{nhel}}$  and  $\eta_t^{\text{hel}}$ , normalized by  $D_0 \equiv u_{\text{rms}}/3k_f$ , for the nonhelical and helical cases, and  $\alpha^{\text{hel}}$  normalized by  $A_0 \equiv u_{\text{rms}}/3$ , for the helical cases for different values of Re. The value of Ma is given for completeness.

Run	Re	$\kappa_t^{\text{nhel}}/D_0$	$\kappa_t^{\text{hel}}/D_0$	$\eta_t^{\text{nhel}}/D_0$	$\eta_t^{\text{hel}}/D_0$	$\alpha^{\text{hel}}/A_0$	Ma <sup>nhel</sup>	Ma <sup>hel</sup>
A	2.4	$1.14 \pm 0.01$	$1.12 \pm 0.01$	$1.12 \pm 0.01$	$0.84 \pm 0.015$	$-0.83 \pm 0.01$	0.062	0.063
B	3.4	$1.47 \pm 0.03$	$1.45 \pm 0.03$	$1.39 \pm 0.02$	$0.97 \pm 0.011$	$-0.95 \pm 0.02$	0.068	0.070
C	5.0	$1.87 \pm 0.04$	$1.93 \pm 0.04$	$1.72 \pm 0.00$	$1.06 \pm 0.03$	$-1.02 \pm 0.02$	0.077	0.081
D	8.7	$2.26 \pm 0.03$	$2.54 \pm 0.01$	$1.96 \pm 0.05$	$1.15 \pm 0.02$	$-0.96 \pm 0.01$	0.089	0.099
E	20.7	$2.54 \pm 0.02$	$2.94 \pm 0.01$	$2.03 \pm 0.03$	$1.40 \pm 0.02$	$-0.83 \pm 0.02$	0.105	0.120
F	45.5	$2.50 \pm 0.03$	$2.82 \pm 0.07$	$1.95 \pm 0.08$	$1.58 \pm 0.16$	$-0.75 \pm 0.03$	0.116	0.128
G	120.6	$2.27 \pm 0.01$	$2.58 \pm 0.12$	$1.73 \pm 0.08$	$1.46 \pm 0.28$	$-0.69 \pm 0.07$	0.123	0.130

**Table 2.** Values of  $\chi_t^{\text{nhel}}$  and  $\chi_t^{\text{hel}}$  normalized by  $D_0 \equiv u_{\text{rms}}/3k_f$ , for the nonhelical and helical cases. The value of Ma is given for completeness.

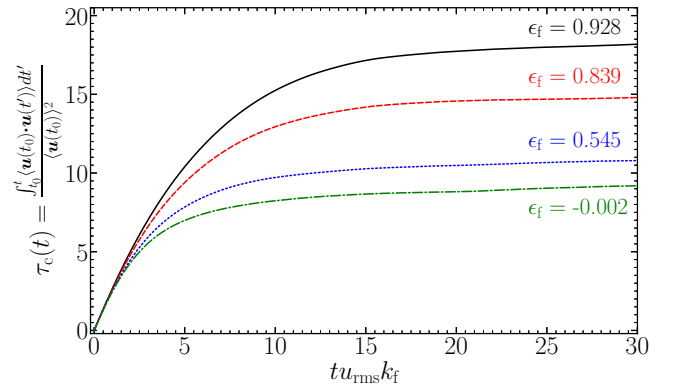
Run	Re	$\chi_t^{\text{nhel}}/D_0$	$\chi_t^{\text{hel}}/D_0$	Ma
A	1.2	$0.63 \pm 0.03$	$0.59 \pm 0.02$	0.031
B	4.7	$1.86 \pm 0.08$	$1.78 \pm 0.09$	0.048
C	11.8	$2.51 \pm 0.05$	$2.72 \pm 0.07$	0.060
D	27.6	$2.57 \pm 0.01$	$2.95 \pm 0.07$	0.070
E	75.1	$2.40 \pm 0.03$	$2.67 \pm 0.04$	0.077
F	151.9	$2.25 \pm 0.02$	$2.52 \pm 0.04$	0.077
G	307.0	$2.18 \pm 0.04$	$2.42 \pm 0.05$	0.078



**Figure 4.** Dependence of  $\chi_t$  for nonhelical (black symbols, solid line) and fully helical turbulence (red symbols, dashed line) as a function of Reynolds number  $\text{Re} = \text{Pe}/\text{Pr}$  with  $\text{Pr} = 1$  in all cases. To make the error bars more visible, they have been exaggerated by a factor of 4.

393 times as the late-time limit of

$$394 \quad \tau_c(t) = \int_{t_0}^t \langle \mathbf{u}(t_0) \cdot \mathbf{u}(t') \rangle dt' / \langle \mathbf{u}^2(t_0) \rangle. \quad (13)$$



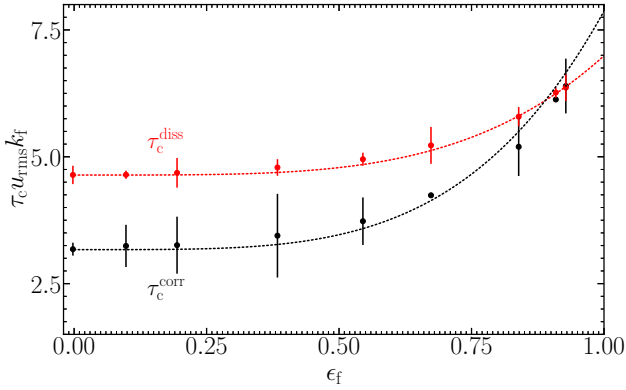
**Figure 5.** Correlation time of turbulence computed from time integrals of velocity autocorrelation from runs with  $\text{Re} = 13$  and different relative helicity  $\epsilon_f = \langle \mathbf{u} \cdot \boldsymbol{\omega} \rangle / k_f u_{\text{rms}}^2$ .

395 The result is shown in Figure 5 for simulations with  
 396  $\text{Re} = 13$  and different values of the relative helicity. We  
 397 see that, through the presence of kinetic helicity, the cor-  
 398 relation time of the turbulent velocity field increases and  
 399 is more than doubled as the kinetic helicity is increased  
 400 from zero to one. We note that the Reynolds number  
 401 of these simulations is very modest. Further studies at  
 402 larger Reynolds numbers would be needed to establish  
 403 the dependence of the correlation time on the kinetic hel-  
 404 icity in more turbulent regimes; see Rogachevskii et al.  
 405 (2025).

406 Another way to estimate the correlation time is ob-  
 407 tained from the ratio of kinetic energy and its dissipation  
 408 rate:

$$409 \quad \tau_c = \frac{E_K}{\epsilon_K}, \quad (14)$$

410 where  $E_K = \frac{1}{2} \langle \mathbf{u}^2 \rangle$  and  $\epsilon_K = 2\nu \langle \mathbf{S}^2 \rangle$ . The results for  
 411 the correlation time are summarized in Figure 6. Both  
 412 measures of  $\tau_c$  show an increasing trend as a function of  
 413 the fractional helicity,  $\epsilon_f = \overline{\mathbf{u} \cdot \boldsymbol{\omega}} / k_f u_{\text{rms}}^2$ .



**Figure 6.** Correlation time  $\tau_c$  as function of  $\epsilon_f$  from the late-time limit of Equation (13) (black symbols) and from Equation (14) (red symbols) normalized by the turnover time  $(u_{rms}k_f)^{-1}$  for the same runs as in Figure 5. The dotted lines are proportional to  $\epsilon_f^4$ , and the error bars are boosted by a factor of ten for  $\tau_c^{diss}$  and by five for  $\tau_c^{corr}$ .

414 Regarding the usage of the energy dissipation rate  $\epsilon_K$   
 415 for the timescale arguments of turbulence, we should  
 416 note the following points. Although developed turbu-  
 417 lence contains a very wide range of scales, it is still  
 418 meaningful to use  $\epsilon_K$  for the arguments of turbulence  
 419 timescale. In the inertial range of fully developed tur-  
 420 bulence, we have a local equilibrium between the pro-  
 421 duction rate of turbulent energy and its dissipation rate.  
 422 In this range, the dissipation rate is equivalent both to  
 423 the energy injection rate at the integral scale and to  
 424 the energy flux (the spectral energy transfer from larger  
 425 scale to smaller scale). In this sense, the energy dissipa-  
 426 tion rate  $\epsilon_K$  is the most appropriate turbulence statisti-  
 427 cal quantity that describes the timescale of turbulence.  
 428 This is the reason why we also adopt  $\epsilon_K$  in the timescale  
 429 argument of turbulence.

430 Turbulent transport coefficients depend on some sta-  
 431 tistical quantities such as the turbulent energy  $E_K$ , its  
 432 dissipation rate  $\epsilon_K$ , kinetic helicity  $H_K$ , etc, as well as  
 433 the time and/or length scales of turbulence, which are  
 434 determined by  $E_K$ ,  $\epsilon_K$  and  $H_K$ , as well as the veloc-  
 435 ity strain rate, vorticity, pressure, etc. Generally, the  
 436 kinetic helicity  $H_K$  depends on the vorticity/rotation  
 437 and density stratification or turbulence inhomogeneity  
 438 as well as the external forcing. Here, for simplicity of  
 439 the argument, we assume that deviations of the turbu-  
 440 lence timescale from the usual eddy turnover time,  
 441  $\tau_c = E_K/\epsilon_K$ , can be expressed in terms of the kinetic  
 442 helicity as  $\tau_c(H_K)$ , and examine the dependence of  $\tau_c$   
 443 on  $H_K$ .

### 444 3.3. Comparisons with the theoretical predictions

445 Let us compare the obtained numerical results with  
 446 the theoretical predictions by Rogachevskii et al. (2025),  
 447 where the path-integral approach for a random velocity  
 448 field with a finite correlation time has been used. Ac-  
 449 cording to the theory, the turbulent magnetic diffusion  
 450 coefficient  $\eta_t(H_K)$  is given by

$$451 \quad \eta_t(H_K) = \eta_{t0} \frac{\tau_c(H_K)}{\tau_0} \left( 1 - \frac{\tau_c^2(H_K)}{3} \frac{H_K^2}{\langle \mathbf{u}^2 \rangle} \right), \quad (15)$$

452 while the turbulent diffusion coefficient  $\kappa_t(H_K)$  of the  
 453 scalar field is

$$454 \quad \kappa_t(H_K) = \kappa_{t0} \frac{\tau_c(H_K)}{\tau_0} \left( 1 - \frac{\tau_c^2(H_K)}{6} \frac{H_K^2}{\langle \mathbf{u}^2 \rangle} \right), \quad (16)$$

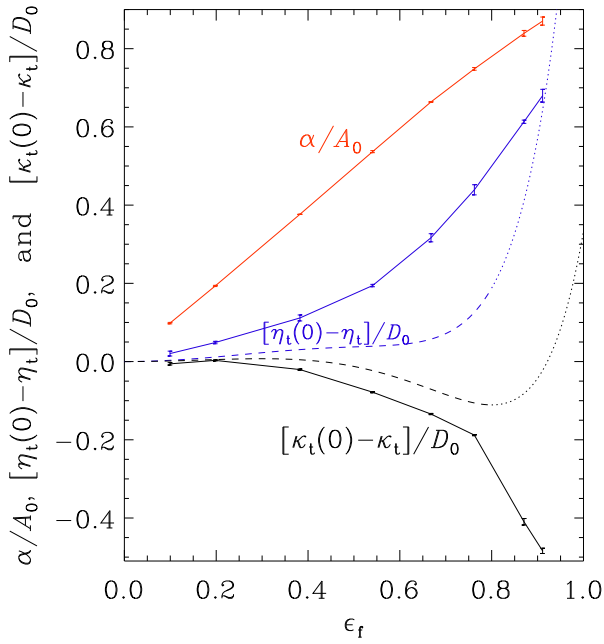
455 where  $H_K = \langle \mathbf{u} \cdot \boldsymbol{\omega} \rangle$ ,  $\eta_{t0} = \eta_t(H_K = 0)$ ,  $\kappa_{t0} = \kappa_t(H_K =$   
 456  $0)$  and  $\tau_0 = \tau_c(H_K = 0) = (u_{rms}k_f)^{-1}$ . Applying two  
 457 independent methods (based on the non-instantaneous  
 458 correlation functions and the rate of energy dissipation)  
 459 for the calculation of the correlation time versus the  
 460 fraction of kinetic helicity, our numerical results suggest  
 461 that

$$462 \quad \tau_c(H_K)/\tau_0 \approx 1 + 0.5\epsilon_f^4. \quad (17)$$

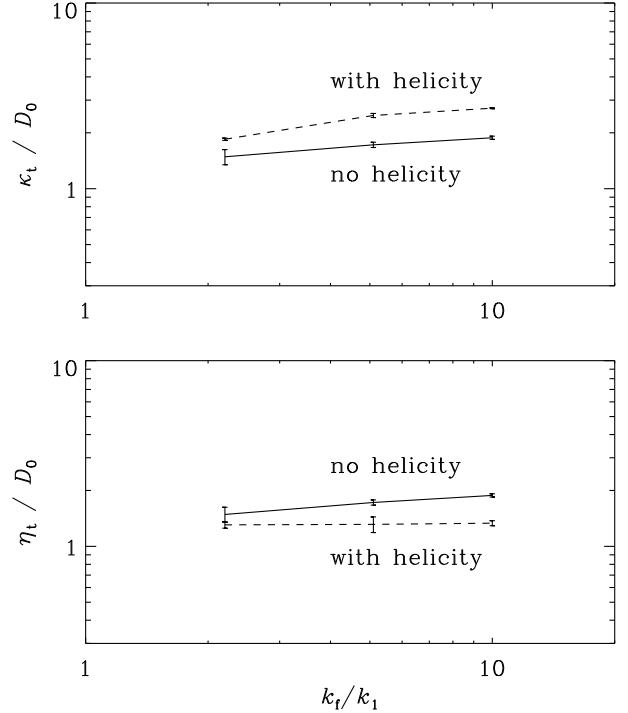
463 Using Equations (15)–(17), we plot in Figure 7 the de-  
 464 pendences  $\eta_t(0) - \eta_t$  and  $\kappa_t(0) - \kappa_t$  on the fraction  
 465  $\epsilon_f$  of the kinetic helicity for  $Re = 13$ . Here,  $\eta_t(0) =$   
 466  $\eta_t(\epsilon_f = 0)$  and  $\kappa_t(0) = \kappa_t(\epsilon_f = 0)$ , and  $\alpha$  is normalized  
 467 by  $A_0 = u_{rms}/3$ , while turbulent diffusion coefficients  
 468 are normalized by  $D_0 = u_{rms}/3k_f$ , where  $k_f$  is the forc-  
 469 ing wavenumber. The theoretical dependencies given  
 470 by Equations (15)–(17) are shown as dashed and dot-  
 471 ted blue and black curves. The theoretical results for  
 472  $\epsilon_f \gtrsim 0.85$  are shown as dotted lines, because they may  
 473 not be reliable.

474 As follows from Figure 7, the turbulent magnetic dif-  
 475 fusion coefficient is reduced by the kinetic helicity, while  
 476 the turbulent diffusion coefficient for the scalar field  
 477 is increased by the kinetic helicity. These arguments  
 478 can explain the results of our direct numerical simula-  
 479 tions; see also Fig. 1 for  $Re = 120$  in Rogachevskii et al.  
 480 (2025).

481 Using an approach based on the Furutsu-Novikov the-  
 482 orem (Furutsu 1963; Novikov 1965), Kishore & Singh  
 483 (2025) found that the turbulent diffusivities of both  
 484 the mean passive scalar and the mean magnetic field  
 485 are suppressed by the kinetic helicity. Note that  
 486 Kishore & Singh (2025) have not taken into account the  
 487 dependence of the correlation time on the kinetic he-  
 488 licity. This may explain the discrepancy with our nu-  
 489 merical results related to the helicity effect on turbulent  
 490 diffusion of the scalar fields.



**Figure 7.** Dependencies of  $\alpha$  (red solid line),  $\eta_t(0) - \eta_t$  (blue solid line) and  $\kappa_t(0) - \kappa_t$  (black solid line) on the fraction  $\epsilon_f$  of the kinetic helicity for  $\text{Re} = 13$ . The theoretical dependencies given by Equations (15)–(17) are shown by dashed and dotted blue and black curves. The theoretical results for  $\epsilon_f \gtrsim 0.85$  are shown as dotted lines, because they may not be reliable.



**Figure 8.** Scale separation dependence of  $\kappa_t$  (upper panel) and  $\eta_t$  (lower panel) for nonhelical (solid lines) and helical (dashed lines). To make the error bars more visible, they have been exaggerated by a factor of 4.

### 3.4. Scale dependence

To assess the scale dependence of the difference of turbulent transport for helical and nonhelical cases, we have varied the ratio  $k_f/k_1$ , keeping the viscosity constant. This implies that  $\text{Re}$  decreases with increasing  $k_f$ . In all cases, we used  $512^3$  meshpoints. The results for helical and nonhelical turbulence are compared in Figure 8 and Table 3. We see that there is a slight increase in the difference between helical and nonhelical cases. For  $\kappa_t$ , however, the difference between helical and nonhelical cases is rather weak. In all cases, we used  $512^3$  meshpoints.

## 4. CONCLUSIONS

Our simulations have revealed a surprising difference in the helicity effect for passive and active scalars on the one hand and magnetic fields on the other. As for magnetic fields, the helicity effect does not exist for small Reynolds numbers. Above Reynolds numbers of about 20, it does not change much any more and there is no indication that it disappears at larger values.

The key numerical result of the present study is the enhancement of turbulent diffusion of the mean passive and active scalar fields by the kinetic helicity. This result is opposite to the magnetic case where turbulent

magnetic diffusion is decreased by the kinetic helicity. We also found that the correlation time of the turbulent velocity field increases because of kinetic helicity. The latter is one of the main points relevant for understanding the kinetic helicity effects on turbulent diffusion of scalar and magnetic fields (see Section 3.3).

The enhancement of the passive scalar diffusion examined here can be compared with the effect of rotation and stratification on the passive scalar diffusivity. As discussed in the introduction, rotating stratified flows also attain kinetic helicity and for such flows, it was previously found that the passive scalar diffusivity gets reduced as the rotation speed is increased, just like the magnetic diffusivity, which also became smaller (Brandenburg et al. 2012). This effect was not ascribed to the presence of helicity, but it was simply regarded as a rotational suppression of the magnetic diffusivity. This difference can probably be explained by the anisotropy of the flow that is being produced in rotating stratified turbulence, which is a more complicated situation than just a helically forced flow.

Qualitatively, one could understand the helicity effect on the magnetic field as a tendency to support dynamo action, or, alternatively, as a tendency for rotational suppression of the magnetic diffusivity. For pas-



**Table 3.** Values of  $\kappa_t^{\text{nhel}}$  and  $\kappa_t^{\text{hel}}$  as well as  $\eta_t^{\text{nhel}}$  and  $\eta_t^{\text{hel}}$ , normalized by  $D_0 \equiv u_{\text{rms}}/3k_f$ , for the nonhelical and helical cases, and  $\alpha^{\text{hel}}$  normalized by  $A_0 \equiv u_{\text{rms}}/3$ , for the helical cases for different values of  $k_f$ . The value of Ma is given for completeness.

Run	$k_f/k_1$	Re	$\kappa_t^{\text{nhel}}/D_0$	$\kappa_t^{\text{hel}}/D_0$	$\eta_t^{\text{nhel}}/D_0$	$\eta_t^{\text{hel}}/D_0$	$\alpha^{\text{hel}}/A_0$	Ma <sup>nhel</sup>	Ma <sup>hel</sup>
a	2.2	281.1	$1.66 \pm 0.03$	$1.85 \pm 0.03$	$1.49 \pm 0.14$	$1.31 \pm 0.05$	$-0.65 \pm 0.01$	0.125	0.131
b	5.1	120.6	$2.27 \pm 0.01$	$2.48 \pm 0.06$	$1.72 \pm 0.06$	$1.31 \pm 0.13$	$-0.69 \pm 0.01$	0.123	0.130
c	10.0	59.3	$2.49 \pm 0.01$	$2.71 \pm 0.02$	$1.88 \pm 0.04$	$1.33 \pm 0.04$	$-0.76 \pm 0.00$	0.119	0.129

540 sive and active scalars, on the other hand, there is no  
 541 dynamo effect. Furthermore, in some special determinis-  
 542 tic flows (the Roberts-IV flow; see Devlen et al. (2013)),  
 543 the effective magnetic diffusivity can even be negative  
 544 and thereby lead to dynamo action. Such an effect  
 545 was never found for passive or active scalars or mag-  
 546 netic fields in turbulent flows at high Reynolds num-  
 547 bers. What has been previously found, however, is a  
 548 suppression of both  $\eta_t$  and  $\kappa_t$  for potential (compress-  
 549 ible) flows (Rädler et al. 2011; Rogachevskii et al. 2018).  
 550 In the present work, however, we have only considered  
 551 nearly incompressible flows for actual turbulence simu-  
 552 lations, as opposed to some constructed flows such as  
 553 the Roberts flow.

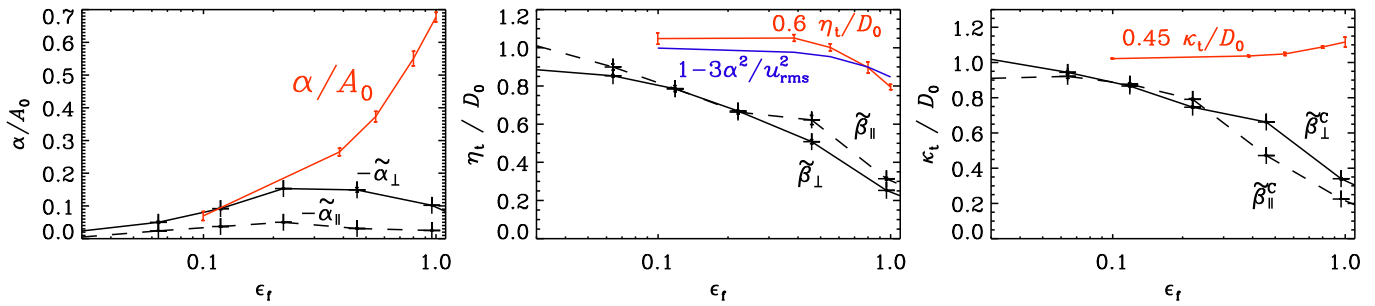
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 575 and Berlin, Germany.

576 *Software and Data Availability.* The source code used  
 577 for the simulations of this study, the PENCIL CODE  
 578 (Pencil Code Collaboration et al. 2021), is available on  
 579 <https://github.com/pencil-code/>. The simulation se-  
 580 tups and corresponding secondary data are available on  
 581 <http://doi.org/10.5281/zenodo.15083000>.

## APPENDIX

### A. COMPARISON WITH EARLIER WORK

583  
 584 In Figure 9, we compare with the values of the  $\alpha$  effect and the turbulent magnetic and passive scalar diffusivities  
 585 from the earlier work of Brandenburg et al. (2012), in which kinetic helicity is being produced by the interaction  
 586 with rotation and stratification. Here, we have estimated the fractional helicity from the product of Coriolis number  
 587  $\text{Co} = 2\Omega/u_{\text{rms}}k_f$  and gravity number  $\text{Gr} = 1/H_\rho k_f$ , where  $\Omega$  is the angular velocity,  $k_f$  is the forcing wavenumber of  
 588 the turbulence, and  $H_\rho$  is the density scale height. We used a formula by Jabbari et al. (2014),  $\epsilon_f = 2\text{CoGr}$ . For the  
 589 present simulations, we used  $\epsilon_f \approx 2\sigma/(1 + \sigma^2)$ .



**Figure 9.** Dependence of the fractional helicity,  $\epsilon_f$ , and comparison of the values of  $\alpha$  and the turbulent magnetic and passive scalar diffusivities with the earlier work of Brandenburg et al. (2012), in which kinetic helicity is being produced by the interaction with rotation and stratification. The originally used symbols of Brandenburg et al. (2012) have been retained:  $-\tilde{\alpha}_\perp$  and  $-\tilde{\alpha}_\parallel$  for the normalized perpendicular and parallel components of the  $\alpha$  effect,  $\tilde{\beta}_\perp$  and  $\tilde{\beta}_\parallel$  for those of the magnetic diffusivity, and  $\tilde{\beta}_\perp^c$  and  $\tilde{\beta}_\parallel^c$  for those of the passive scalar diffusivity. The tildes indicate appropriate normalization. In the second panel, we also show in blue  $1 - 3\alpha^2/u_{\text{rms}}^2$ .

590 There is not much agreement with our present simulations, shown in red. This shows that other effects such as the  
 591 rotational suppression of turbulent transport plays a more dominant role than just the helicity.

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